

Differential Joints or Circumferential Joint

$$\textcircled{i} \quad t = \frac{p_i D_i}{2\sigma + m} + 1 \\ = 21 \text{ Nm.}$$

$$\textcircled{ii} \quad d = 6 \sqrt{F} \\ = 28 \text{ Nm.}$$

$$\textcircled{iii} \quad n = \left(\frac{p}{\sigma}\right)^2 \cdot \frac{p}{F} \\ = \left(\frac{2400}{28}\right)^2 \cdot \frac{1}{56} \\ = 132 \text{ rivets.}$$

(iv) Pitch of Rivets :-

Assume joint be double riveted lap joints.

No. of Rows = 2.

$$n_1 = \text{no. of rivets per Row} = \frac{n}{2} = 66.$$

$$\text{Pitch, } p_i = \frac{(D_i + t)}{n_1} = \frac{(2400 + 21)}{66} \\ = 115.2 \text{ Nm}$$

$$p_{\max.} = (t + 41.28)$$

$$= 2.62(21) + 41.28$$

$$= 96.3.$$

$$\therefore p = 96 \text{ Nm}$$

Assuming Zig-Zag Riveting :-

$$p_t = 0.33(p) + 0.67d,$$

$$= 0.33(96) + 0.67(28)$$

$$= 50.44 \text{ Nm.}$$

$$m = 1.5(d)$$

$$= 42 \text{ Nm}$$

over lap, q

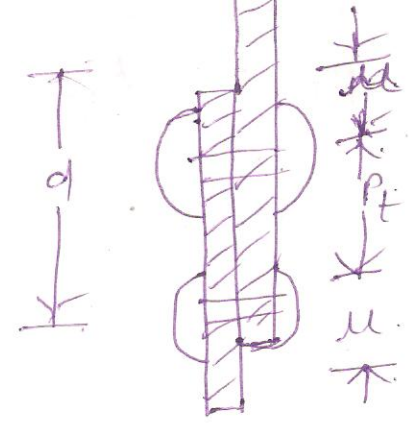
$$P_t + 2u$$

$$= 50 \cdot 4u + 2(4u)$$

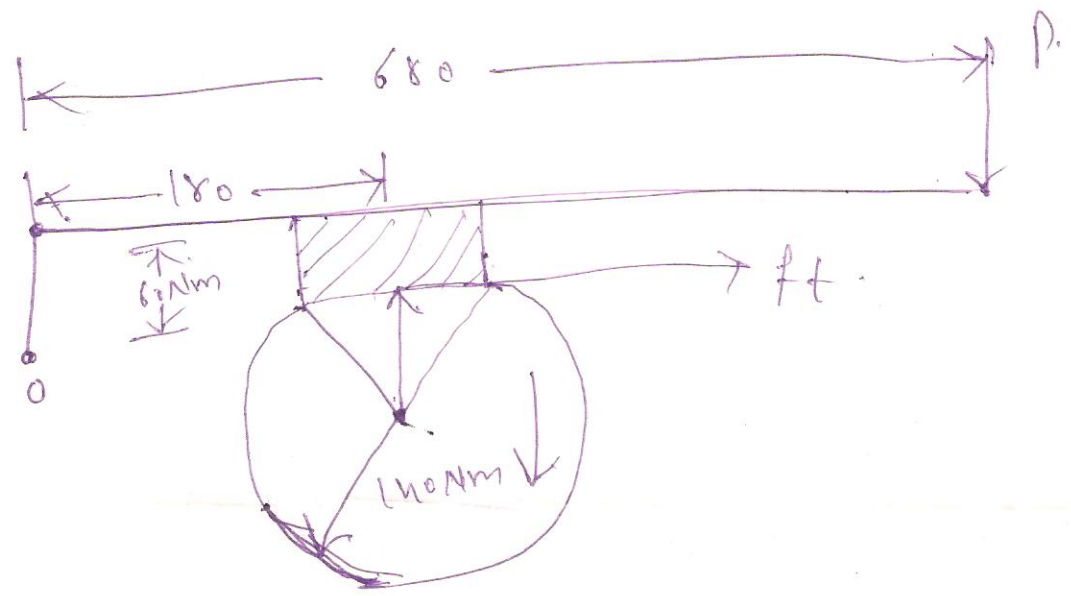
$$= 134 \text{ Nm}$$

$$\eta_i = \frac{P - d}{P} = \frac{46 - 28}{96}$$

$$= 70.83\%$$



A=4



Given

$$T = 15 \text{ N-m}$$

$$\mu = 0.3$$

$$P_{max} = 14 \text{ N/mm}^2$$

$$u = d$$

$$T = P_t \times r$$

$$15 = \mu R_N \cdot \frac{140}{1000}$$

$$\frac{15}{0.3 \times 0.14} = R_N$$

$$R_N = 357.143 \text{ N}$$

Taking $\Sigma M @ 0$:

$$P \times 680 + P_t \times 0.6 = R_N \times 180$$

$$P \times 68 + (0.3 \times 357.143) \times 0.6 = 357.143 \times 18$$

$$P \times 68 = 64.28 - 6.43$$

$$P = 85.07 \text{ N}$$

(ii) Block Design :-
 $PB = \frac{RN}{A}$

$$\frac{1N}{Nm^2} \Rightarrow \frac{357.143 N}{W(28 \sin \theta)}$$

Here θ is Not Given but, we may use $w = d$

$$w = d$$

$$w = 28 \sin \theta$$

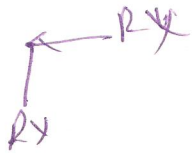
$$\therefore w = 2 \times 140 \times \sin 2\theta$$

$$= 255 Nm$$

(let $2\theta = 40^\circ$)

(iii)

Resultant Hinge Pin Reaction :-



$$R_y = -P + RN$$

$$= 85 + 357$$

$$= 272 N$$

$$R_x \Rightarrow F_t = \mu RN$$

$$= 0.3 \times 357$$

$$= 107 N$$

(iv)

Heat Generation Rate :-

$$N = 50 \text{ r.p.m}$$

$$H.G.R = F_t \times V$$

$$= 107 \times \pi \times 28 \times 50$$

$$= \frac{78.4 J}{\text{sec}}$$

A=6

KNUCKLE JOINT

$$P = 150 \text{ KN} = 150 \times 10^3$$

$$\sigma_t = 80 \text{ MPa}$$

$$t = 60 \text{ MPa}$$

$$\sigma_c = 158 \text{ MPa}$$

(i) Dia of Rod (D) :-

$$D = \sqrt{\frac{4P}{\pi \sigma_t}} = \sqrt{\frac{4 \times 150 \times 10^3}{\pi (80)}}$$

$$= 48.86 \text{ mm}$$

$$(ii) D_1 = 1.1 D \\ = 53.75 \text{ Nm}$$

$$(iii) a = .75 \times 48.86 = 36.64 \text{ Nm} \\ b = 1.25 \times 48.86 = 61.08 \text{ Nm}$$

$$(iv) \text{ pin dia } :- \\ d = \sqrt{\frac{2P}{\pi t}} = \sqrt{\frac{2 \times 150 \times 10^3}{\pi \times 60}} \\ = 39.9 \text{ Nm}$$

$$d = 3 \sqrt{\frac{32}{\pi \times b} \times \frac{P}{2} \left[\frac{b}{4} + \frac{a}{3} \right]} \\ = 3 \sqrt{\frac{32}{\pi (80)} \times \frac{150 \times 10^3}{2} \left[\frac{61}{4} + \frac{36}{3} \right]} \\ = 63.8 \text{ Nm}$$

$$\therefore d = 63.8 \text{ Nm}$$

$$d_o = 2 \times d = 127.7 \text{ Nm} \\ d_i = 1.5d = 95.7 \text{ Nm}$$

$$(v) \text{ CHECK } \sigma_t = \frac{P}{b(d_o - d)} \\ = \frac{150 \times 10^3}{61(127.7 - 63.8)} \\ = 38.48 \text{ MPa}$$

\therefore safe

$$\sigma_c = \frac{P}{b d} \\ = \frac{150 \times 10^3}{61 \times 63.8} \\ = 38.54 \text{ MPa}$$

\therefore safe