

where  $h = 1.135$  for dry saturated steam

$P_1 =$  pre. of steam at entry in  $N/m^2$  absolute.

$V_1 =$  vol. of one kg. of steam at pre.  $P_1$  in  $m^3$

$P_2 =$  pre. of steam  $N/m^2$  abs.

$A =$  Area of cross section ( $m^2$ ) of nozzle at the throat.

$V_2 =$  vol. of one kg. of steam at absolute pre.  $P_2$

Now there is only one value of the ratio ( $P_2/P_1$ ) to which the discharge of steam through the nozzle is maxm. The value ( $P_2/P_1$ ) is called critical pre. ratio. Therefore we differentiate only that portion which is inside the square brackets & equate it to zero.

$$i.e. \frac{2}{n} \left(\frac{P_2}{P_1}\right)^{2/n-1} - \frac{h+1}{n} \left(\frac{P_2}{P_1}\right)^{h/n-1} = 0 \text{ or } \frac{2}{n} \left(\frac{P_2}{P_1}\right)^{\frac{2-h}{n}-\frac{h+1}{n}} = 0$$

$$= \left(\frac{P_2}{P_1}\right)^{\frac{2-h}{n}-\frac{h+1}{n}} = \frac{h+1}{n} \times \frac{n}{2} = \frac{h+1}{2}$$

$$\Rightarrow \left(\frac{P_2}{P_1}\right)^{\frac{1-h}{n}} = \frac{h+1}{2} = \left(\frac{2}{h+1}\right)^{-1} \text{ or } \frac{P_2}{P_1} = \left(\frac{2}{h+1}\right)^{-\frac{n}{1-h}}$$

$$\Rightarrow \left(\frac{P_2}{P_1}\right) = \left(\frac{2}{h+1}\right)^{\frac{h}{n-1}} \Rightarrow \frac{P_2}{P_1} = \left(\frac{2}{h+1}\right)^{\frac{h}{n-1}}$$

now for dry saturated is 1.135 & critical pre. ratio is 0.518.

It may be defined as the ratio of isentropic head drop in the moving blades to isentropic head drop at the reaction turbine.

Two degree of reaction (R) =  $\frac{\text{Enthalpy drop in moving blades} = h_2 - h_3}{\text{Enthalpy drop in stage} = h_1 - h_3}$

=  $\frac{\text{Increase in the relative K.E in moving blade}}{\text{Stage work output}}$

$$\frac{V_{r0}^2 - V_{r1}^2}{V_b(V_{w1} - V_{w0})} = \frac{V_{v0}^2 - V_{v1}^2}{2 V_b (V_{w1} - V_{w0})}$$

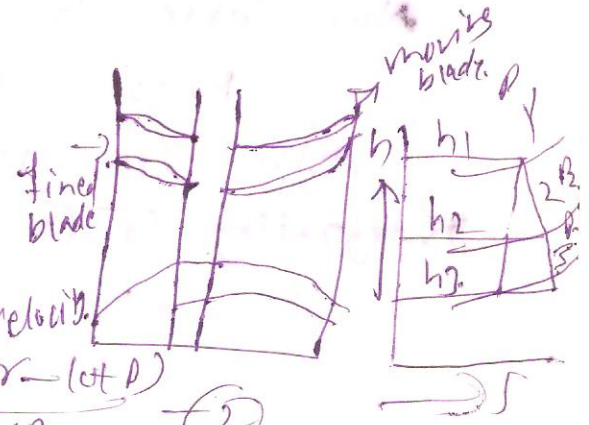
Stage work output

$V_{r0} = V_f \cos \alpha$  &  $V_{r1} = V_f \cos \beta$

$V_{w1} + V_{w0} = V_f (\cos \beta + \cos \alpha)$

$V_f =$  vel. of flow which remains constt. through the stages

$$\therefore R = \frac{V_f^2 (\cos^2 \alpha - V_f^2 \cos^2 \beta)}{2 V_f (\cos \beta + \cos \alpha) V_b} = \frac{V_f (\cos \alpha - \cos \beta)}{2 V_b} \quad (2)$$



For 50% degree of reaction  $V_b = V_f (\cos \alpha - \cos \beta)$  (3)

from the vel. triangle  $V_b$  can also be expressed as under

$$V_b = V_f (\cos \alpha - \cos \beta) = V_f (\cos \alpha - \cos \beta) \quad (4)$$



